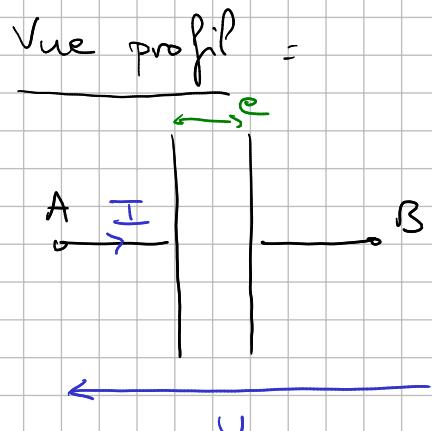
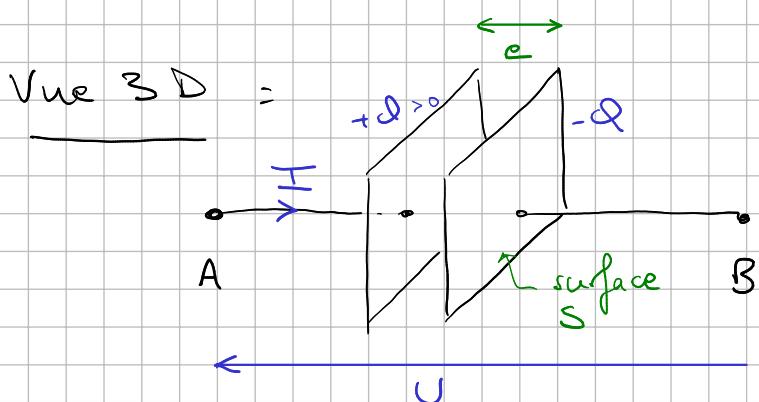


## Condensateur plan

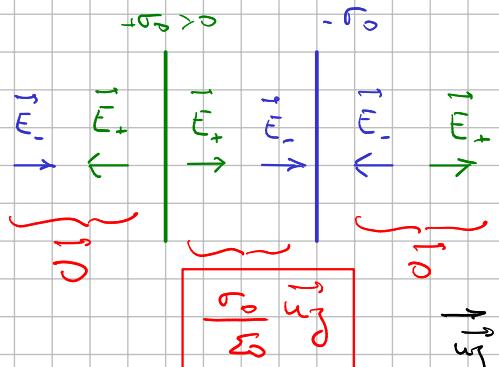
1.1-



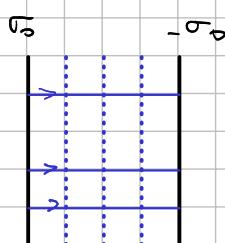
- Armatures chargées uniformément  $\sigma_0 = \frac{f}{S} > 0$
  - Si besoin, parce que  $S \gg e^2$ , on pourra considérer armatures  $\infty$ .

$$1.2. \text{ Rappel} : \left\| \vec{E} \right\| = \frac{\left| \sigma_0 \right|}{2 \varepsilon_0} \text{ pour plan } \infty$$

2



→ l'd chps + équipots :



$$\int_A^B \vec{E} \cdot d\vec{l} = V_A - V_B \Rightarrow U = \frac{\sigma_0}{\Sigma} e \quad \|\vec{E}\| = \frac{U}{e}$$

$$\boxed{(\text{ou})} \quad \vec{E} = -\vec{\text{grad}} V \Rightarrow \begin{vmatrix} 0 \\ \frac{\partial V}{\partial x} \\ \frac{\partial V}{\partial y} \\ \frac{\partial V}{\partial z} \end{vmatrix} = - \begin{vmatrix} \frac{\partial V}{\partial x} \\ \frac{\partial V}{\partial y} \\ \frac{\partial V}{\partial z} \end{vmatrix} \Rightarrow \frac{\partial V}{\partial j} = - \frac{\sigma_0}{\epsilon_0}$$

$$\Rightarrow V(g) = -\frac{r_0}{|g|} + C^k$$

$$\underline{\text{Climites}} = \begin{cases} V(j=\omega) = V_A \\ V(j=e) = V_B \end{cases} \Rightarrow \frac{V_A - V_B}{\xi_0} e.$$

$$1.3. \text{ Déf}^p C = Q \stackrel{\text{def}}{=} C U$$

$$\text{Ici } U = \frac{\tau_0}{\varepsilon_0} e \quad \text{or } \tau_0 = \frac{Q}{S} \Rightarrow U = \frac{Q}{S \varepsilon_0} e$$

$$Q = \frac{\varepsilon_0 S}{e} U$$

$$C = \varepsilon_0 \frac{S}{e}$$

F      Fm<sup>-1</sup>

1.4. Si milieu DL Mi à la place du vide interarmature,  
au air

alors  $\varepsilon_0 \rightarrow \varepsilon$ .  $\varepsilon_{\text{air}} \approx 80 \varepsilon_0$  !

NB : attent au chp disruptif. air :  $3 \text{ MV.m}^{-1}$

1.5. Energie EM stockée dans  $\vec{E}$  interarmature :

$$E_{\text{stock}} = \iiint \varepsilon_0 \frac{\|\vec{E}\|^2}{2} d\tau = \frac{\varepsilon_0}{2} \frac{U^2}{e^2} (S \times e) = \frac{1}{2} \left( \frac{\varepsilon_0 S}{e} \right) U^2$$

tout l'espace  
 où il y a chp  
 élec.

$$= \frac{1}{2} C U^2$$